

TIME-INVARIANT ADJOINT NETWORKS: GENERALIZED DESCRIPTION FORMULATION*

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ABSTRACT

The adjoint network is developed through the allowed pair formulation of networks and shown to yield a general description representation in the time-invariant case.

I. INTRODUCTION

Since Bordewijk [1] introduced the concept of interreciprocity as applied to electrical networks, the adjoint network has played an important role in Computer Aided Design [2] and network sensitivity [3]. Its description has recently been developed in terms of general descriptions on graphs by Desoer [4].

In this paper a formulation of the adjoint network N^a is outlined in terms of the definition [5] of an n -port network N through its allowed pairs of voltage and current, $[v, i] \in N$. This is developed for any linear time-invariant network having the frequency domain general description $AV = BI$, amplifying the idea of Desoer. Moreover, the general description for the adjoint network N^a is found.

II. FORMULATION OF THE ADJOINT NETWORK

Given an n -port network defined through its set of allowed time-domain voltage - current pairs $[v, i] \in N$, [5, p.7], with v and i the n -vectors of port voltages and currents, we define the adjoint n -port network N^a by $[v^a, i^a] \in N^a$ if and only if for all $[v, i] \in N$ and all t and τ

$$[\tilde{v}(t), I(t)] \begin{bmatrix} i^a(\tau) \\ -v^a(\tau) \end{bmatrix} = 0 \quad (1)$$

where $\tilde{}$ denotes the transpose. Let $t = x - \tau$ and

and integrate over τ to get convolution in (1). On taking Laplace transforms this gives in the frequency domain

$$[\tilde{V}(p), \tilde{I}(p)] \begin{bmatrix} I^a(p) \\ -V^a(p) \end{bmatrix} = 0 \quad (2)$$

If N is linear and characterized in the frequency domain by the general description

$$AV = BI \quad (3)$$

then we can similarly characterize N^a as follows: Equation (3) implies

$$[A, -B] \begin{bmatrix} V \\ I \end{bmatrix} = 0_{n \times 1}$$

or equivalently on transposing

$$[\tilde{V}, \tilde{I}] \begin{bmatrix} \tilde{A} \\ -\tilde{B} \end{bmatrix} = 0_{1 \times n} \quad (4)$$

Multiplying by an arbitrary n -vector X , Equation (4) gives

$$[\tilde{V}, \tilde{I}] \begin{bmatrix} \tilde{A} \\ -\tilde{B} \end{bmatrix} X = 0 \quad (5)$$

On identifying with Equation (2)

$$I^a = \tilde{A}X \quad (6a)$$

$$V^a = \tilde{B}X \quad (6b)$$

III. GENERAL DESCRIPTION OF THE ADJOINT NETWORK

By finding a common left multiple M of \tilde{A} and \tilde{B} for Equations (6), following [6, p.35,36] (as illustrated by the example below), we obtain

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$$[B^a, A^a] \begin{bmatrix} \tilde{A} \\ -\tilde{B} \end{bmatrix} = 0_{n \times n} \quad (7a)$$

or

$$M = B^a \tilde{A} - A^a \tilde{B} \quad (7b)$$

where $[B^a, A^a]$ has rank n , the maximum possible rank. Thus, for these matrices B^a and A^a in p , Equations (6) give

$$B^a I^a = B^a \tilde{A} X - M X = A^a \tilde{B} X = A^a V^a \quad (8)$$

The general description of the adjoint network N^a is thus established as

$$B^a I^a = A^a V^a \quad (9)$$

which completely describes the adjoint network in view of the rank n condition satisfied by $[B^a, A^a]$ as mentioned above.

Example

A current controlled current source has

$$AV = \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ \beta & -1 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = BI$$

We form, with the W matrix nonsingular, using elementary row and column operations

$$\begin{bmatrix} W_{11} & W_{12} \\ W_{21} & W_{22} \end{bmatrix} \begin{bmatrix} \tilde{A} & 0 \\ -\tilde{B} & 0 \end{bmatrix} = \begin{bmatrix} D & 0_n \\ 0_n & 0_n \end{bmatrix}$$

from which

$$W_{21} \tilde{A} = W_{22} \tilde{B}$$

In the case of our example

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -1 & -\beta \\ 0 & 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & -\beta & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

or, extracting the 2×2 (2,1) submatrix,

$$\begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix} = \begin{bmatrix} -1 & -\beta \\ 0 & 0 \end{bmatrix} \begin{bmatrix} 0 & \beta \\ 0 & -1 \end{bmatrix}$$

Multiplying by X on the right gives, from (6)

$$\begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} i_1^a \\ i_2^a \end{bmatrix} = \begin{bmatrix} -1 & -\beta \\ 0 & 0 \end{bmatrix} \begin{bmatrix} v_1^a \\ v_2^a \end{bmatrix}$$

which is a (reversed) voltage controlled voltage source. The circuits are as shown in Figure 1.

IV. CONCLUSIONS

We have extended in a straightforward manner the approach of Desoer for formulating the adjoint network. This establishes the constraint $B^a I^a = A^a V^a$ for N^a directly from the port variable definition of the original network N in the frequency domain without reference to the network graph. The time-variable case will be developed elsewhere because it is too lengthy to present here. The formulation here, though, when applied to the special cases of Z , Y , and H descriptions, gives the classical results, $Z^a = \tilde{Z}$, $Y^a = \tilde{Y}$, and $H^a = \tilde{H}$, respectively.

V. REFERENCES

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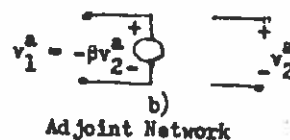
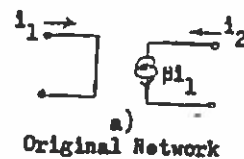


Figure 1
Example Circuits

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