

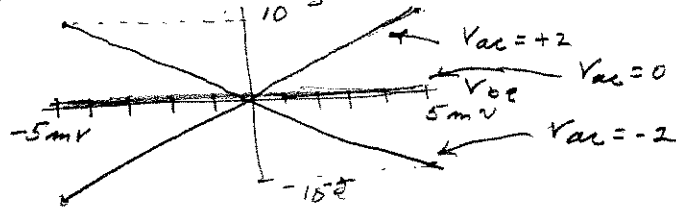
#1.  $\frac{I_B}{\beta} = \frac{V_{ac} V_{bc}}{1 + 0.001 |V_{bc}|}$  is odd in  $V_{bc}$  for a fixed  $V_{ac}$  of which there are 3.

for  $V_{bc} > 0$   $\frac{I_B}{\beta} = \frac{-2 \times 10^{-3} V_{bc}}{1 + 0.001 V_{bc}}$ , 0,  $\frac{+2 \times 10^{-3} V_{bc}}{1 + 0.001 V_{bc}}$  and over  $-5mV < V_{bc} < 5mV$   
 $0.001 \times 5 \times 10^{-3} = 5 \times 10^{-6}$   
 is much smaller than 1 & can be ignored (for larger  $V_{bc}$  it keeps  $I_B$  bound)

∴ over  $-5mV < V_{bc} < 5mV$

$\frac{I_B}{\beta} \approx -2 V_{bc} \times 10^{-3}$ , 0,  $+2 V_{bc} \times 10^{-3}$

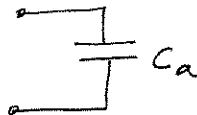
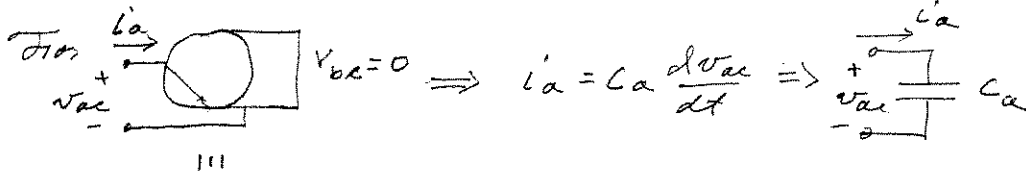
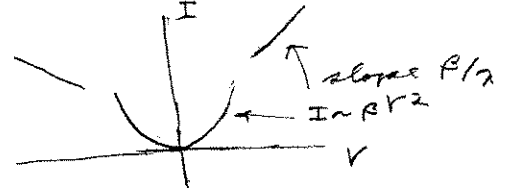
a)



For the connection of b),  $V_{ac} = V_{bc} = V$ ,  $I_B = I = \beta \frac{V^2}{1 + 2|V|}$

near  $V=0$ ,  $I \sim \beta V^2 \sim$

b) as  $V \rightarrow \pm\infty$ ,  $I \sim \frac{\beta}{2} |V|$



#2. When  $I_a = I_b$  there is complete symmetry about a vertical line through the middle of  $I_T$ , so

a)  $I_{D_{Ma_2}} = I_{D_{Mb_2}} = \frac{1}{2} I_T$ , so  $I_c = I_{D_{Mb_2}} - I_{D_{Ma_2}} = \underline{\underline{0}} = I_c$

For part b), if  $I_a = 1mA$  the drain of  $M_{a_1}$  will be at its highest potential while if at the same time  $I_b = 0mA$  the drain of  $M_{b_1}$  will be ground potential (so  $M_{b_1}$  is turned off),

thus all of  $I_T$  goes through  $M_{a_2}$  so that  $I_{D_{Ma_2}} = I_T$ ,  $I_{D_{Mb_2}} = 0 \Rightarrow I_c = I_{D_{Mb_2}} - I_{D_{Ma_2}} = -I_T$

By symmetry, when  $I_a = 0$ ,  $I_b = 1mA$ , then  $I_{D_{Mb_2}} = I_T$ ,  $I_{D_{Ma_2}} = 0 \Rightarrow I_c = I_{D_{Mb_2}} - I_{D_{Ma_2}} = I_T$

The table is thus

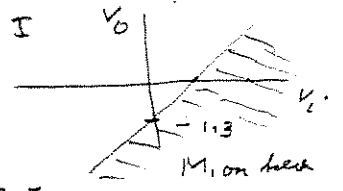
b)

$I_a$	$I_b$	$I_c$	$ I_c $
0	0	0	0mA $\Rightarrow$ 0
1mA $\Rightarrow$ 1	1mA $\Rightarrow$ 1	0	0mA $\Rightarrow$ 0
1mA $\Rightarrow$ 1	0	-1mA	1mA $\Rightarrow$ 1
0	1mA $\Rightarrow$ 1	1mA	1mA $\Rightarrow$ 1

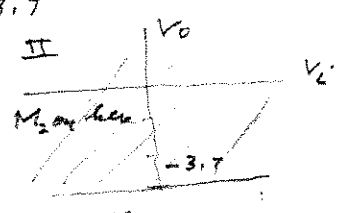
c) Thus  $|I_c|$  is the XOR of  $I_a$  &  $I_b$  when treated as representations of binary numbers

#3.

For  $M_1$  on,  $V_{GS1} = V_i - V_0 \geq V_{TO_n} = 1.3 \Rightarrow V_0 \leq V_i - 1.3$



For  $M_2$  on,  $V_{GS2} = V_0 - V_{DD} \geq V_{TO_n} \Rightarrow V_0 \geq V_{DD} + V_{TO_n} = -5 + 1.3 = -3.7$

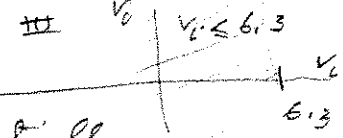


$\therefore M_1$  &  $M_2$  both on in  $-3.7 \leq V_0 \leq V_i - 1.3$

For  $M_1$  in saturation (& on)  $0 \leq V_{GS1} - V_{TO_n} \leq V_{DS1}$

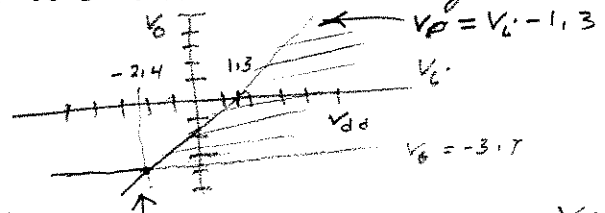
which is  $0 \leq V_i - V_0 - V_{TO_n} \leq V_{DD} - V_0$

$\Rightarrow V_i \leq V_{DD} + V_{TO_n} = 5 + 1.3 = 6.3 \Rightarrow$



For  $M_2$  in saturation (& on), region II is automatically true

The region for both transistors on & in saturation we have the intersection of regions I, II, III



intersection  $V_0 = -3.7 = V_i - 1.3 \Rightarrow V_i = -2.4$

a)  $\therefore$  For  $-2.4 \leq V_i \leq 6.3$   $M_1$  &  $M_2 =$  on & sat.

In this region  $I_{D_{M1}} = I_{D_{M2}}$  which is

$$\frac{K_{P1}W}{2L} (V_i - V_0 - V_{TO_n})^2 = \frac{K_{P2}W}{2L} (V_0 - V_{DD} - V_{TO_n})^2$$

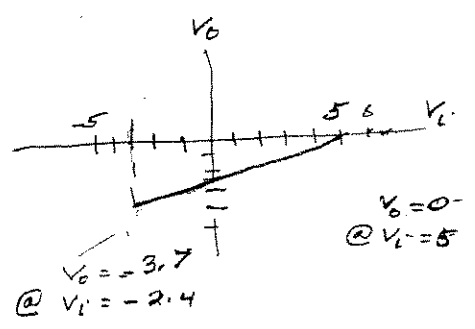
Using the + square root as both  $M_1$  &  $M_2$  are on

$$V_i - V_0 - V_{TO_n} = V_0 - V_{DD} - V_{TO_n}$$

which is  $2V_0 = V_i + V_{DD} = V_i + 5$

or  $V_0 = \frac{1}{2}V_i + 2.5$

b)



c) although  $V_0 < 0$  when  $V_i > 0$  this does not give a sharp transition or a strong zero or one, so it is not a good digital inverter. Since  $\frac{dV_0}{dV_i} > 0$  this is not a good small signal inverter, as it does not invert.