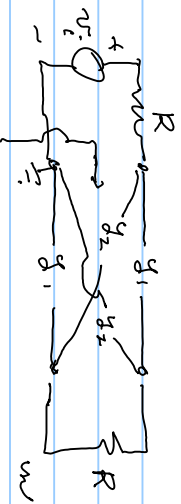


Constant R lattices



R at input Load



$$i = Y v = \begin{bmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$y_{11} = \frac{i_1}{v_1} \Big|_{v_2=0}$$

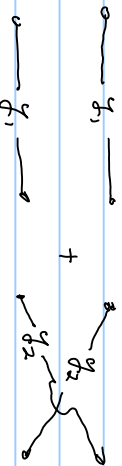
$$y_{12} = \frac{i_1}{v_2} \Big|_{v_1=0}$$

$$y_{21} = y_{11}$$

try symmetry

$$y_{21} = \frac{i_2}{v_1} \Big|_{v_2=0}$$

$$Y = \frac{1}{2} \begin{bmatrix} g_1 + g_2 & g_2 - g_1 \\ g_2 - g_1 & g_2 + g_1 \end{bmatrix}$$



$$Y = \begin{bmatrix} \frac{g_2}{2} & -\frac{g_1}{2} \\ -\frac{g_1}{2} & \frac{g_2}{2} \end{bmatrix}$$

$$Y = \begin{bmatrix} \frac{g_2}{2} + \frac{g_2}{2} & \\ & \frac{g_2}{2} \end{bmatrix}$$

$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} i_1' \\ -i_2' \end{bmatrix}$$

$$-y_{12}v_2 = y_{21}v_1 + y_{22}v_2 \Rightarrow -(y_{12} + y_{22})v_2 = y_{21}v_1$$

$$\frac{v_2}{v_1} = -\frac{y_{21}}{y_{12} + y_{22}}$$

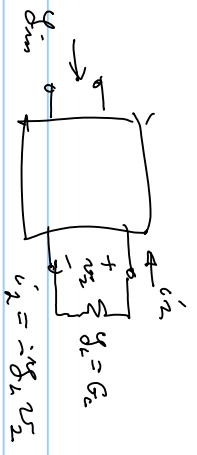
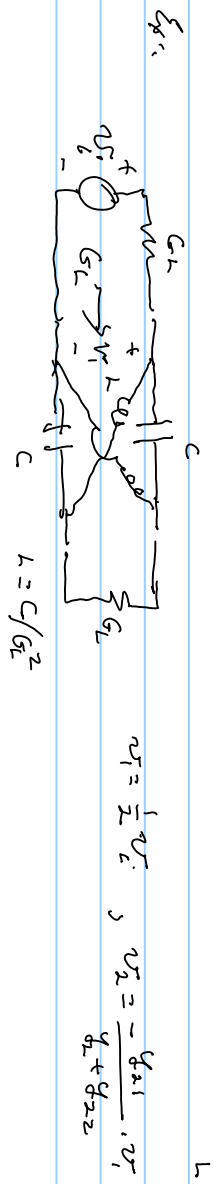
$$i_1 = y_{11}v_1 + y_{12}v_2 = y_{11}v_1 + y_{12} \cdot \frac{(-y_{21})}{y_{12} + y_{22}} \cdot v_1 = \left[ \frac{y_{11}y_{22} + y_{12}y_{21}}{y_{12} + y_{22}} - y_{12} \frac{y_{21}}{y_{12} + y_{22}} \right] v_1$$

$$y_{in} = \frac{\text{det } Y + y_{12}y_{21}}{y_{12} + y_{22}} \Rightarrow \text{constant } R \Rightarrow y_{in} = G_n, y = G_L$$

$\Rightarrow G_L^2 = \text{det } Y$  but  $y_{22} = y_{11}$  for the circuit asymmetric lattice

$$= y_{11}y_{22} - y_{12}y_{21} = y_{11}^2 - y_{12}^2 = \frac{1}{4}(y_1 + y_2)^2 - \frac{1}{4}(y_2 - y_1)^2 = \frac{1}{4} [y_1^2 + 2y_1y_2 + y_2^2 - (y_2^2 - 2y_1y_2 + y_1^2)] = \frac{1}{4} \frac{4y_1y_2}{4}$$

$$\Rightarrow \text{constant } R, G_L^2 = y_1y_2 \Rightarrow y_2 = G_L^2/y_1 \quad \text{So: } y_1 = AC \quad \text{Then } y_2 = \frac{G_L^2}{AC} = \frac{1}{AL}$$



$$y_1 = \frac{1}{2}(y_2 - y_1), \quad y_2 = \frac{1}{2}(y_2 + y_1) \Rightarrow \frac{v_2}{v_1} = \frac{-\frac{1}{2}(y_2 - y_1)}{G_2 + \frac{1}{2}(y_2 + y_1)} = \frac{y_1 - y_2}{2G_2 + (y_2 + y_1)}$$

But  $y_2 y_1 = G_1^2 \Rightarrow y_2 = \frac{G_1^2}{y_1} \Rightarrow \frac{v_2}{v_1} = \frac{y_1 - G_1^2/y_1}{2G_2 + (G_1^2/y_1 + G_1^2)} = \frac{y_1^2 - G_1^2}{2G_2 y_1 + G_1^2}$

$$\frac{v_2}{v_1} = \frac{(y_1 - G_2)(y_1 + G_2)}{(y_1 + G_2)^2} = \frac{y_1 - G_2}{y_1 + G_2} \quad \text{if } y_1(j\omega) = jB(\omega), \quad B(\omega) \text{ real}$$

Then  $\frac{v_2}{v_1}(j\omega) = \frac{-G_2 + jB(\omega)}{G_2 + jB(\omega)} = \frac{|-G_2 + jB(\omega)| e^{j \arctan(-G_2/B(\omega))}}{|G_2 + jB(\omega)| e^{j \arctan(G_2/B(\omega))}}$

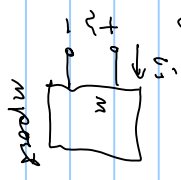
$$y_1(s) = sC$$

↑ all pass; changes phase

can cascade keeping constant R & then the gains multiply & keeps all pass

Passivity:  $E(t) \geq 0$  for all time  
 || energy into the circuit =

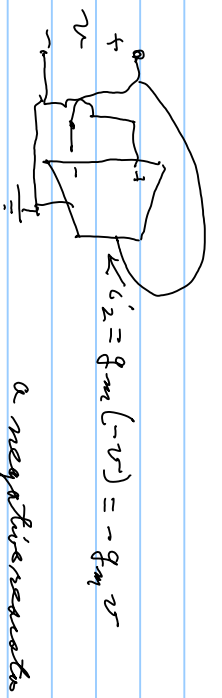
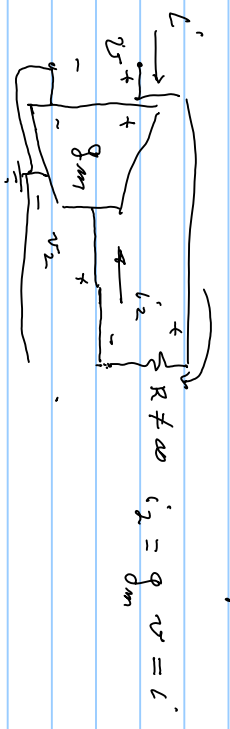
$$P(t) = \int_{-\infty}^t v^T(\tau) i(\tau) d\tau \geq 0$$



$$i_1 = G v_1, \quad 1/R = G$$

$$G = \text{const.}$$

$$\int_{-\infty}^t v_1 G dt = G \int_{-\infty}^t v_1 dt = G \times \text{positive if } v_1 > 0$$

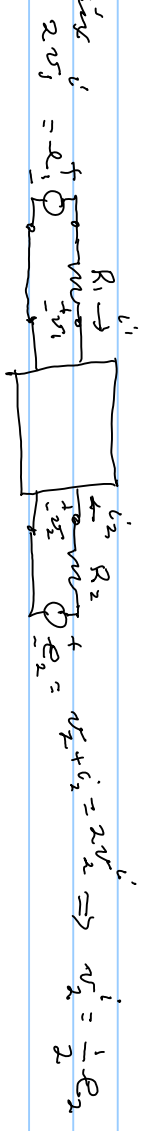


operational Transconductance amplifiers (G component in Series)

$G < 0 \Leftrightarrow R < 0$  for this connection

$\Rightarrow$  OTA is not possible as it gives a negative resistor

characterizing matrices



$2v_1 = v_1 + R i_1 = \text{incident}$

$2v_2 = v_2 - R i_2 = \text{reflected}$

$R = \begin{bmatrix} R_1 & 0 \\ 0 & R_2 \end{bmatrix}, \quad R_1 \geq 0, R_2 \geq 0$

normally to  $R = 1/2$

$2v_1 = v_1 + v_1 \Rightarrow v_1 = v_1 + v_1$

$2v_2 = v_2 - v_2 \Rightarrow v_2 = v_2 - v_2$

S = scattering matrix:  $v^R = S v^L$ ;  $S_{21} = \frac{v_2^R}{v_1^L} \Big|_{v_2^L=0} = \frac{(v_2 - i v_2)/2}{v_1/2} = v_2^R$

$S_{11} = \frac{v_1^R}{v_1^L} \Big|_{v_2^L=0} = \text{reflection coefficient @ port 1}$   
 when load in  $R_2$   
 $v_2^R = 0 = \frac{(v_2 - i v_2)/2}{(v_1 + i v_1)/2} = \frac{1 - i v_1/v_1}{1 + i v_1/v_1} = \frac{1 - \gamma_{in}}{1 + \gamma_{in}}$   
 when load port 2,  $R_2 = 1$   
 $S_{11} = \frac{-v_2^R}{v_1^L} = \text{voltage gain, loaded in } R_2 = 1$

Before  $A(v^L)v^R = B(v^L)v^R$

$v^R = v^{L'} + v^R \Rightarrow A(v^{L'} + v^R) = B(v^{L'} - v^R)$   
 $v = v^{L'} - v^R \Rightarrow (A - B)v^{L'} = (-A - B)v^R \Rightarrow (B + A)v^R = (B - A)v^{L'}$   
 $v^R = S v^{L'}$

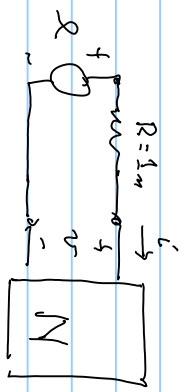
$S = (B + A)^{-1} (B - A)$ ; if  $i = Y v \Rightarrow A = Y, B = 1_m$

$= (1_m + Y)^{-1} (1_m - Y)$

note if  $Y$  comes from a passive network diagonal entry = -1 or  $(1_m + Y)^{-1}$  exists

choose  $R$  such that  $\int_{-\infty}^t e^{i\tau} e^{i\tau} d\tau$  is finite  $\forall \tau$

$e = (v + i) \Rightarrow e(t) = \int_{-\infty}^t (v^T + i^T + 2v^T) d\tau \quad \tau > 0, e \in \mathcal{L}^2_{loc}$



∴ of Nois process  $\int_{a_0}^t r^T_i \geq 0$  Then as  $\int_{0,t} r^T dx \geq 0$  if  $r \in \mathcal{I}^2_{[0,t]}$   
with  $\int_{0,t} r^T dx \geq 0$  &  $\int_{0,t} r^T dx \geq 0$  &  $\int_{0,t} r^T dx \geq 0$  &  $\int_{0,t} r^T dx \geq 0$